RESEARCH ARTICLE



In situ X-ray tomographic microscopy observations of vesiculation of bubble-free and bubble-bearing magmas

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Abstract Magma degassing is thought to play a major role in magma fractionation, transport, storage, and volcanic eruption dynamics. However, the conditions that determine when and how magma degassing operates prior to and during an eruption remain poorly constrained. We performed experiments to explore if the initial presence of gas bubbles in magma influences the capability of gas to escape from the magma. Vesiculation of natural H₂O-poor (<<1 wt.%) silicic obsidian glasses was investigated by in situ, high-temperature (above the glass transition) experiments using synchrotron-based X-ray tomographic microscopy with high spatial (3 μ m/pixel) and temporal resolution (1 second per 3D dataset). As a validation, a second set of experiments was performed on identical starting materials using a Karl-Fisher titration setup to

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quantify the amount of extracted gas that escapes via volatile diffusion and/or bubble coalescence during vesiculation. In both sets of experiments, vesiculation was triggered by heating the samples at room pressure. Our results suggest that the presence of pre-existing gas bubbles during a nucleation event significantly decreases the tendency of bubbles to coalesce and inhibits magma outgassing. In contrast, in initially bubble-free samples, the nucleation and growth of bubbles is accompanied by significant coalescence and outgassing. We infer that volatile-undersaturated (i.e. bubble-free) magmas in the reservoirs are more likely to erupt effusively, while the presence of excess gas already at depth (i.e. bubble-bearing systems) increases the likelihood of explosive eruptions.

 $\label{eq:constraint} \begin{array}{l} \mbox{Keywords} \ \mbox{Magmas} \cdot \mbox{Vesiculation} \cdot \mbox{Bubbles} \cdot \mbox{Degassing} \cdot \mbox{Outgassing} \cdot \mbox{Synchrotron} \cdot \mbox{X-ray} \cdot \mbox{Experiments} \cdot \mbox{Volcanic} \\ \mbox{eruption style} \end{array}$

Introduction

The style and intensity of a volcanic eruption can be strongly affected by the efficiency of gas removal during the ascent of magma to the surface (Sparks 2003, and references therein). Gas exsolution in combination with increasing magma viscosity tends to generate overpressure in the gas bubbles, and if the excess gas is not readily removed from magma in this runaway process, an explosive eruption may occur (e.g. Melnik et al. 2005). The release of excess volatiles is fundamentally controlled by the coalescence of gas bubbles, the development of gas permeability, and magma brittle fracturing in the periods immediately preceding and/or occurring during an eruption. However, determining the numerous details and factors interacting and regulating the ability of magmas to degas is inherently complex because such processes occur at depth and

in timescales that are not accessible with conventional experimental techniques, where the analysis of bubble textures is performed post-mortem, i.e. after gas escape and melt quenching, and, thus, after original gas bubbles become vesicles. Further, one of the fundamental questions of volcanology is whether or not it is possible to predict the likelihood of effusive versus explosive eruptions on the basis of the physical properties of magmas, such as rheology, volatile content, and rate of volatile exsolution (Fisher and Schmincke 1984).

Several experimental studies have been conducted to explore the mechanisms of gas exsolution and permeability (e.g. Larsen et al. 2004; Burgisser and Gardner 2005; Takeuchi et al. 2005) and to determine the conditions required for magma fragmentation (e.g. Mangan and Sisson 2000; Namiki and Manga 2005). Yet, in these studies only the final run products, representing the last "frame" of a dynamic process (e.g. Pistone et al. 2012, 2013). were analysed. Pioneering experiments, combining high-temperature devices and X-ray tomographic microscopy, have significantly contributed to understanding bubble formation and growth in basaltic (Bai et al. 2008; Baker et al. 2012) and felsic (Gondé et al. 2011; Okumura et al. 2013) systems, but have thus far not focused on the effect of pre-existing gas bubbles on the development of permeability.

In this study, we performed experiments at magmatic temperatures observing the vesiculation of bubbles and the development of gas permeability in three spatial dimensions and time (i.e. 4D), using a novel technique developed at the TOMCAT beamline of the Swiss Light Source at the Paul Scherrer Institut (Villigen, Switzerland; Stampanoni et al. 2006; Mokso et al. 2010; Fife et al. 2012; Pistone et al. 2015). In these experiments, we stimulate gas exsolution by increasing temperature for samples of different chemistries. In general, decompression is the principal cause of magma vesiculation during volcanic eruptions. Although our experiments do not simulate magma decompression, they nevertheless offer important insights into the dynamics of magma vesiculation in SiO2-rich systems and constrain how the initial volatile saturation conditions of magmas (i.e. the presence or absence of gas bubbles) can potentially affect the style of degassing and, thus, the style of a volcanic eruption.

Experimental and analytical techniques

Starting materials and Karl-Fischer titration

Five natural samples of obsidian were selected as starting materials:

- Two samples from Lipari Island (Acqua Calda, LIP, and Rocche Rosse, LIP2, Aeolian Islands, Italy; Gottsmann and Dingwell 2001)
- A sample from Little Glass Mountain (Medicine Lake Highland, California, USA; LGM; Fink 1983)

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- A sample from Mayor Island (New Zealand; MI; Stevenson et al. 1993)
- A sample from Las Cañadas Caldera (Tenerife, Canary Islands, Spain; CAN; Fife et al. 2012; Madonna et al. 2013).

LIP, LIP2 and LGM are bubble-free, whereas MI and CAN are bubble-bearing (bubble fraction, β =0.02 in MI, and β = 0.04 in CAN; bubble fraction estimated by three-dimensional analysis; see below). LIP, LIP2, LGM, and MI are metaluminous rhyolites in the TAS diagram (Le Maitre et al. 2002; Fig. 1) whereas the CAN sample is a peralkaline phonolite (see also Table 1A in Appendix).

The initial H_2O contents of the samples (LIP=0.54 wt.%; LIP2=0.25 wt.%; LGM=0.10 wt.%; MI=0.24 wt.%; CAN= 0.23 wt.%) and the amounts of H2O extracted at different temperatures were determined by Karl-Fischer titration (KFT; Fischer 1935; Behrens et al. 1996) using a CA 100 Moisture Meter (COSA Instruments, Mitsubishi Chemical Corporation), which uses high purity argon stream as carrier transporting H₂O from the heated sample to the titration cell. Samples were heated up from 573 to 1523 K at constant heating rate of 2 K/s (for fine-grained powders) to 10 K/s (for glasses) using a Linn High Therm HTG-REG controller, and a total titration time of minutes was applied during KFT analysis. Precision and accuracy of the equipment were tested by calibration measurements, with an individual measurement error of $\pm 0.003-0.005$ wt.%, and a precision of replicate analysis of ±0.05 wt.% H₂O (Pistone et al. 2012, 2015). Since the melt viscosity (η_{melt}) of the samples was rather high ($\eta_{melt} > 10^5$ Pa·s at<1523 K), to determine the total initial H₂O content of the samples, finegrained powders of the samples were mixed with $Li_2B_4O_7$ powder (Merck Chemicals, Switzerland), with a ratio of 1:5. During analysis this procedure lowers the liquidus temperatures of the glasses, their viscosities and enables complete H₂O extraction from the melt even at low water contents, which promote slow diffusion (Zhang et al. 1991; Behrens et al. 1996). Since Li₂B₄O₇ is extremely hygroscopic, KFT analyses began at 573 K to avoid contamination by adsorbed H2O from external moisture. The residual H₂O in Li₂B₄O₇ was separately determined at various temperatures and used to correct the H₂O content of the single sample in the same temperature range. KFT measurements were additionally performed on glass cylinders with dimensions similar to those used for the X-ray tomographic microscopy experiments (see next paragraph) to quantify the amount of H₂O released from the samples during bubble nucleation and growth.

The main samples of this study are LIP and MI, which were chosen as proxies for volatile-undersaturated (bubble-free LIP) and volatile-saturated magmas (bubble-bearing MI, β = 0.02). Differently from the microstructural analyses reported in the work of Rust et al. (2003). the MI sample displays an initial average bubble size of 10–20 µm and bubbles having



Fig. 1 TAS diagram (Le Maitre et al. 2002, modified) displaying the natural obsidian samples investigated in this contribution. *Black dots* indicate the primary samples simulating volatile-undersaturated (LIP) and volatile-saturated (MI) systems, respectively. *Grey dots* indicate the samples testing the effect of composition (CAN), the initial H₂O content (LIP2) and the presence of chemical heterogeneities (i.e. Fe-Ti oxides; LGM) on gas exsolution. Specifically, the CAN and LGM samples are

used for comparison with the MI and LIP samples, respectively. Abbreviations: ϕ =solid crystal volume fraction; β =gas bubble volume fraction; H_2O =initial H₂O content dissolved in the glass phase, expressed in wt.%. Reported data are volatile-free basis. The different samples display the following agapatic indices (i.e. molar ratio Al₂O₃/[Na₂O+ K₂O]): LIP and LIP2=1.03; MI=1.16; LGM=1.27; CAN=0.96

an aspect ratio of 2-5. The additional samples (LIP2, LGM, and CAN) served to test: (i) the influence of chemical composition (CAN, β =0.04 with initial average bubble sizes of 10–20 μ m and aspect ratios of 2–5; cf. MI); (ii) the effects of initial H₂O content (LIP2, 0.25 wt.% H₂O and bubble-free, cf. LIP); and (iii) to evaluate the effect of the presence of microcrystals in the starting material (LGM, 0.1 wt.% H₂O and 1 vol.% 1-5 µm-sized Fe-Ti oxides; cf. LIP and MI) on gas exsolution (Fig. 1). In the bubble-bearing samples (MI and CAN), the distance between bubbles prior to the experiments exceeded 10 µm and, therefore, can be assumed that the bubble-bubble distance is sufficient enough to hamper eased bubble coalescence. The difference in initial H₂O contents between the LIP and LIP2 samples may possibly be related to different amounts of molecular H₂O, which may be higher in the LIP sample since it was collected from an obsidian outcrop located close to a hot spring (Acqua Calda, Lipari, Italy).

In order to investigate glass chemical and textural homogeneity, samples were inspected using a Hitachi S-3500 N scanning electron microscope (SEM; University of Bristol, UK). Figure 2 reveals minor inhomogeneities of K, Na, and Ca (<2 %) in the glass composition of the LIP sample, which may potentially behave as sites for bubble nucleation. None of the other obsidian samples displays significant internal variations in glass composition, which is a prerequisite to study the primary impact of the presence *or* absence of initial bubbles on subsequent gas exsolution simulated in these experiments. To minimise such chemical and physical variations in the same sample, we drilled sample cores (2 mm outer diameter and 2 mm length) in portions of the natural obsidian glasses displaying homogeneous aspect (e.g. bands of larger size than the sample core). Minor differences in the chemical properties between the samples (e.g. alkalis content, initial H_2O content) could also contribute to differences in the behaviour of bubble nucleation and growth (i.e. local heterogeneous bubble nucleation) observed during experiments.

Because viscosity differences, along with volatile diffusivity (Sparks et al. 1994). tend to affect the bubble nucleation rate (Murase and McBirney 1973). care was taken that the samples employed in this study have similar melt viscosities (i.e. less than 2 log units in η_{melt} difference in the range 10^5 – 10^{13} Pa · s; see next section) in the temperature window investigated. Utilising relatively high viscosity ($\eta_{melt} > 10^5 \text{ Pa} \cdot \text{s}$) materials has several advantages, most importantly their difficulty to crystallise at super solidus temperatures and their relatively sluggish bubble nucleation and growth kinetics that allowed for capturing 4D image sequences with minimal movement artefacts during X-ray tomographic microscopy upon continuously-increasing temperature (see next section). Finally, the low H₂O content of our samples permitted us to focus on melts with initial super solidus viscosities (η_{melt}) 10^{5} Pa·s) that are characteristic for the pre-fragmentation stage in volcanic eruptions of SiO₂-rich systems.

Experimental setup and synchrotron-based X-ray tomographic microscopy

Samples for the 4D X-ray tomographic microscopy experiments were obtained by drilling cylindrical cores of 2 mm **Fig. 2** Back scattered electron (BSE) and characteristic EDSbased X-ray distribution maps of the LIP sample obtained by SEM at 25 kV acceleration voltage and 10 nA beam current. *Colour scales* of the X-ray distribution maps are expressed in wt.%. Maps reveal minor chemical variability (Ca, K, Na) that are not found in the other natural obsidian glasses used in this study



outer diameter and 2 mm length from the natural obsidians. The sample was then inserted into a hot-pressed boron nitride (BN) holder (4 mm outer diameter, 2.2 mm inner diameter; Fig. 3), which was attached to a zirconia rod on the rotation stage at the TOMCAT beamline of the Swiss Light Source. BN is used as the sample holder because it is largely X-ray transparent and features excellent thermal and chemical stability (up to 1273 K in air) and relatively high thermal conductivity (20–60 Wm^{-1} K⁻¹; Wiley-VCH 1999; Mortazavi et al. 2015). The sample is predominantly homogeneous, with no major variations in the bubble volume fraction or size distribution along the length of the specimen; thus, heat transfer to the sample through the BN wall (0.9 mm thickness) appeared to be rapid and efficient. Using Fourier's law of heat conduction, a minimal temperature differential (<10 K) was calculated along the height of sample as long as the sample remained within the BN holder (5 mm height). Radial thermal gradients are considered even lower due to continuous rotation during X-ray tomographic microscopy acquisition and the sample located at the centre of the X-shaped laser setup (Fife et al. 2012). In cases where the sample expanded outside the BN holder (such as 'mi2 ' in Table 1B in the Appendix), the protruding portion was almost certainly at a lower temperature than the rest of the sample and therefore excluded from subsequent analyses.

Data were acquired using the ultra-fast endstation at the TOMCAT beamline (Stampanoni et al. 2006; Mokso et al. 2010) coupled with the laser-based heating system available at TOMCAT (Fife et al. 2012). This setup utilises a high-flux

source of polychromatic X-rays or "white beam" radiation filtered to 5 % power and the high speed pco.DIMAX camera with a tunable microscope adjusted to approximately four times magnification. As such, a 3D dataset consisting of 1000 projections were captured over 180° of rotation in 1 s with an isotropic pixel size of 2.96μ m. Two different acquisition modes were employed to ultimately capture the dynamics of bubble evolution: (1) a single scan of the sample acquired at a single temperature; and (2) continuous scans of the sample during heating at a specified rate. All experiments were conducted above the glass transition temperature of the respective samples (LIP=885 K; MI=865 K; CAN=849 K; LGM=975 K; as estimated using the model of Giordano et al. 2008). sample LIP2 was not investigated in the X-ray tomographic microscopy experiments.

Laser-based heating system

The laser-based heating system, developed by Fife et al. (2012). is composed of two near-infrared (IR) diode lasers, operating at a wavelength of 980 nm and a maximum power output of 150 W each (Apollo Instruments, Irvine, CA, USA). Each laser illuminates a rectangular spot of 0.2 mm high \times 1-mm wide at the proper working distance of the optics, which can spread to larger spot sizes depending on the size of the specimen placed in the laser paths. We utilised a sample holder made of BN, which essentially worked as high-temperature furnace during the experiments (Fig. 3). Two visible laser spots are used to determine the location of the laser heating



Fig. 3 (a) Schematic and **(b)** actual images of the experimental setup used in combination with the ultra-fast data acquisition endstation (Mokso et al. 2010) and the laser-based heating system (Fife et al. 2012) at the TOMCAT beamline (Stampanoni et al. 2006)

on the sample. The temperature is recorded by a non-contact pyrometer (Optris; Berlin, Germany). The pyrometer is a class 2 IR laser that filters out IR and near-IR wavelengths such that the diode lasers are invisible to the temperature reading. The pyrometer records the temperature of the sample within its line-of-sight based on thermal changes in its spot, within 0.1 K in the range of 623–1973 K (Fife et al. 2012).

Three-dimensional microstructural analysis

The 4D (3D+time) tomographic datasets were processed using a collection of different tools for quantitative analysis and visualisation. To convert the original tomographic projections into binary images, a simple grey levels threshold was combined with morphological operations as described in Mader et al. (2012). For surface-based analyses, customised codes in Interactive Data Language (IDL) were used. The 3D renderings were made with both IDL and Avizo[®] software (Visualization Sciences Group). For the quantitative analysis of volumetric shapes and features, a custom set of algorithms that labelled individual regions of the cellular material (i.e. gas bubbles) were used (Mader et al. 2012). To calculate these metrics, a shape tensor was computed for each bubble. The shape tensors were calculated using covariance of the voxel positions belonging to each bubble (Mader et al. 2012, and references therein). The tensor was visualised as an ellipsoid with 3 principal axes (eigenvectors) and 3 lengths for each axis (eigenvalues). The degree of anisotropy was calculated as the ratio of the difference between the longest and shortest axes and the longest axis of the bubble, with the latter resulting in a number between 0 (spherical) and 1 (infinite). From these metrics, specific values for bubble dimensions, radii, bubble connectivities, and anisotropies were quantified and compared. When applied to a time series of dynamic data, the movements, volumes, and anisotropies of individual gas bubbles could be tracked with increasing time and temperature. The resulting 4D microstructure evolutions of samples LIP and MI can be seen in Movies 1 and 2, respectively (see Appendix). The volume fraction of bubbles (β) in the sample is determined as the ratio between the volume of bubbles and the total sample volume (volume of bubbles+volume of melt; Gardner et al. 1999).

Results

KFT experiments

The results obtained for the extraction of H₂O from glass cylinders reveal many similarities but also some striking differences between samples (Fig. 4). Heating glass cylinders of the Lipari obsidians (LIP and LIP2) resulted in the progressive loss of about 0.14 wt.% H₂O corresponding to 26 % extraction of the total initially dissolved H₂O (LIP, Fig. 4a). Conversely, no detectible amount of H₂O is extracted from the glass cylinder of sample LGM (Fig. 4a). Measurements performed on glass cylinders of samples MI and CAN under identical conditions, also did not record any H2O extraction from the samples during heating (Fig. 4b). Interestingly, the samples with the lower calculated η_{melt} are the samples where no H₂O was extracted during heating, except LGM sample (Fig. 4c). For all powdered samples, the total amount of H₂O extracted is significantly larger than the amount extracted from glass cylinders, and we consider the final value of H2O released at the highest temperature (1523 K) as the total H₂O content of the specimens. Based on the melt chemistry and KFT-measured H_2O content, η_{melt} for each sample was calculated using the model of Giordano et al. (2008). η_{melt} of each sample decreases with temperature by 5 orders of magnitude within the temperature window of the tomography experiments (grey area in Fig. 4c). The range of isothermal η_{melt} of all samples does not exceed more than 2 log units (Fig. 4c) at all temperatures considered.



(*) = Conditions of the in situ 4D high-temperature synchrotron-based X-ray tomographic microscopy experiments at the TOMCAT beamline of SLS

Fig. 4 Amounts of extracted H₂O as measured by Karl-Fisher titration (KFT) at different temperatures (*T*) in a fine-powdered sample and in solid glass cylinders of the: (a) LIP, LIP2 and LGM; and (b) MI and CAN samples. The *image insets* in **a** and **b** are 2D X-ray projection images of the LIP and MI samples before and after heating. (c) The evolution of melt viscosity (η_{melt}) as a function of *T* for the CAN, LIP and MI specimens, with η_{melt} estimated using the model of Giordano et al. (2008). and considering the H₂O content in the residual melt for a specified *T*, taken from the amounts of extracted H₂O in **a** and **b**. The *inset images* in **c** show 3D renderings of post-mortem microstructures of the LIP, MI and CAN samples. I_0 and I_f reported in the *inset images* in **a** and **b** indicate initial and final lengths of the LIP and MI samples before and after heating, respectively. The *grey-coloured areas* in **a**, **b**, and **c** represent the temperature range of the dynamic X-ray tomographic microscopy experiments

X-ray tomographic microscopy experiments

The 3D tomographic renderings illustrate the profound change of bubble texture during heating (Fig. 5) recorded by continuous image acquisition (Movies 1–2). No crystallisation occurred during vesiculation in any sample. It should be noted that Fig. 5d is a rendering of the bubbles present in the MI sample prior to heating, whereas all other renderings in Fig. 5 are those of the melt phase.

The final microstructure of the LIP sample after heating (Fig. 5c) reveals a distribution of gas bubbles including large unconnected sub-spherical bubbles and relicts of gas channels composed of vertically elongated small bubbles. The generation of gas channels by bubble coalescence is confirmed by the increase of bubble anisotropy in the LIP sample at the initial stage of heating (Fig. 6a). The peak anisotropy at 1088 K is associated with an increase of β up to almost 0.4 (Fig. 6a). Most bubble nucleation and growth occurred between 1073 K (starting temperature) and 1088 K, which generated a dramatic increase in vesicularity from bubble-free to β =0.35 (Fig. 6a). The dynamics of this initial burst of vesiculation was too rapid to be captured on the timescale of the data acquisition; this, together with the simultaneous dominant bubble coalescence process, which could have "overwritten" the signature of the initial bubble nucleation and growth, does not allow us to confirm if incipient heterogeneous bubble nucleation operated at the initial stage of vesiculation in the LIP sample. As the temperature increases to 1103 K, the anisotropy significantly decreases; meanwhile, β increases slowly to 0.47 (Fig. 6a). With further heating to 1268 K, the slow and modest increase of β is explained by a further increase in the volume of gas being largely accommodated by permeable flow out of the sample. The β and number of bubbles continuously evolve but these changes were minor compared to the initial microstructure changes up to 1088 K despite the substantial loss of H₂O over the duration of vesiculation as recorded by the KFT experiments (Fig. 4a).

In the LIP sample, diffuse bubble coalescence occurs predominantly through melt film thinning by stretching between expanding gas bubbles (Castro et al. 2012; Fig. 5a-c; Movie 1). In addition, bubble coalescence is the controlling process generating gas channels (see image insets in Figs. 4c and 6a) that serve as permeable pathways for gas escape. Further expansion of the remaining unconnected bubbles, bubble-poor sample portions, and loci of previous degassing pathways suffer local deformation (see the yellow-boxed portion of the LIP sample in Fig. 5a-c and Movie 1, representing a shear band composed of stretched 100 µm long bubbles), generating fabrics similar to those observed in natural pumices (Klug et al. 2002; Wright and Weinberg 2009). Overall, bubble connectivity induced by bubble coalescence in the LIP sample introduces anisotropy (Fig. 6a), which masks the simultaneous isotropic expansion of gas bubbles. Bubble coalescence and outgassing can further be detected by analysing the bubble number density (BND=number of bubbles per melt volume; Gaonac'h et al. 2005) as a function of temperature (Fig. 7a). BND in the LIP sample stays nearly constant for the experimental duration starting from 1188 K (Fig. 6a) due to the competition between bubble coalescence and gas removal (that should decrease BND) and nucleation and growth of novel gas bubbles (that should increase BND). The extent of bubble coalescence and gas loss in the LIP sample are consistent with the trend of cumulative 3D BND (Fig. 7b).

The evolution of bubble textures observed in the MI sample during heating is very different from the observations of the LIP sample and can be attributed to two principal processes: (i) change of shape of pre-existing prolate bubbles towards spherical bubbles (up to 967 K) and (ii) nucleation and growth of new gas bubbles (Fig. 6b). Gas expansion promotes strong vertical inflation of the sample, which results in a foam structure that is at least twice the initial length and volume of the original sample (see the inset images in Fig. 4b). During heating, the central portion of the MI sample transforms into a mono-dispersed bubbly suspension, with gas bubbles having an average diameter of about 200-300 µm (Fig. 5d-f; Movie 2). Bubbles are not interconnected but instead impinge on each other along melt films and at the three neighbouring bubble edges or *Plateau borders* that separate the melt films (Bikerman 1973; Kraynik 1988). This generates a polygonal network (see image inset in Fig. 4c), which resembles the structures found in felsic frothy pumices. A thin melt film is assumed to separate the bubbles and prevent coalescence (Fig. 5d-f; Movie 2), although at the spatial resolution of the scans (approximately 9 µm, based on a minimum of three pixels [2.96 µm/pixel] representing a feature in the microstructure), this may not be adequately resolved. The absence of significant outgassing is furthermore evidenced by the large increase of bubble fraction from 0.02 to 0.87, accompanied by a change in bubble shape from prolate to sub-spherical at 1057 K (Fig. 6b, Movie 2). The slight increase of the bubbles anisotropy at the highest temperatures (1207–1297 K; Fig. 6b) is due to the vertical expansion of the sample (inset in Fig. 6b)

Fig. 5 3D renderings of: (a–c) the LIP sample, showing the melt phase in green while the bubbles are transparent; and (d-f) the MI sample, showing the melt phase in gold while the bubbles are transparent (except in d where, because bubble volume fraction is low, the bubbles are shown in gold and the melt is transparent). The bottom right corner of each subfigure indicates the temperature (T) and the bubble fraction (β) for the image. The yellow-boxed portions in the LIP sample subfigures highlight bubble coalescence (a), outgassing (b), and shear banding of residual bubbles that were not outgassed (c). The 3D renderings of the LIP and MI samples are based on the dynamic experiments carried out at the TOMCAT beamline. Specifically, heating rates were: 15 K/s in the temperature range 1073-1268 K for the LIP sample and 28 K/s in the temperature range 907-1303 K for the MI sample. 3D renderings of the CAN sample are reported in the studies of Fife et al. (2012) and Madonna et al. (2013). 3D renderings of the LGM sample are reported in Pistone (2012). The LIP2 sample was not investigated in the X-ray tomographic microscopy experiments



and bubble impingement at β >0.74. BND in the MI sample sharply increases from 967 to 1147 K, followed by a slight decrease to 1237 K, and stabilises until the end of the run (Fig. 7c). Between 1147 and 1237 K, the decrease of BND can be associated with local bubble connectivity not accompanied by gas removal (Fig. 6b). The general trend of the cumulative 3D bubble size distribution suggests that nucleation and growth of bubbles via gas expansion dominate during heating (Fig. 7d). The volume concentration of larger bubbles increases (radius of 110–130 μ m), and a wide distribution of bubble sizes between 90 and 130 μ m (about 70 vol.%) develops, which strongly differs from the initial bubble size distribution (Fig. 8a).

The LGM and CAN samples used in this study display different behaviour during gas exsolution compared to the LIP and MI samples. The LGM sample only exhibits very limited bubble nucleation and growth ($\beta < 0.03$) close to the sample periphery, with no observable bubble anisotropy (Fig. 6a). No microlites of

Fig. 6 Absolute bubble anisotropy (red and orange lines) and bubble volume fraction (light and dark green dots) as a function of temperature for: (a) LIP and LGM; and (b) MI and CAN samples. Schematic drawings highlight the principal microstructural results during high temperature vesiculation. The *image inset* in **a** provides a 3D rendering of the LIP sample containing a gas channel promoting outgassing (see red arrow). The image inset in b reveals the large expansion of the MI sample during vesiculation



Fe-Ti oxide can be detected at the spatial resolution of the X-ray tomographic microscopy experiments (2.96 µm/pixel); thus, we are not able to quantify the dynamics of heterogeneous bubble nucleation and growth from preferential microlite sites, as it was observed in previous studies (e.g. Hurwitz and Navon 1994). The CAN sample displays a polygonal network of gas bubbles similar to that of the MI sample (see image inset in Fig. 4c; additional textural information can be found in the studies of Fife et al. 2012, and Madonna et al. 2013) when $\beta \sim 0.65$ (Fig. 6b). However, the CAN sample experiences a sharp increase of vesiculation similar to that of the LIP sample, with an initial gas burst followed by a smooth increase of β up to 0.74 when gas bubbles start to impinge on each other (Fig. 6b). Residual bubble anisotropy is observed even at the highest temperature (Fig. 6b).

Discussion

Bubble nucleation and growth in highly viscous, water-poor silicic magmas

The rate of bubble growth is a function of the concentration of volatiles, rate of gas diffusion, viscosity of the surrounding melt, bubble surface tension, and gas overpressure (Gonnermann and Manga 2007, and references therein). At constant pressure and in stationary melt, two processes control bubble growth: (i) diffusion of H_2O molecules from the bulk of the supersaturated melt towards the bubble-melt interface (diffusion-limited bubble growth); and (ii) expansion of the bubble by viscous deformation of the surrounding melt (viscosity-limited bubble growth; Navon et al. 1998). The



Fig. 7 Bubble number density (BND) as a function of temperature for: (a) LIP, and (c) MI samples. Representative 2D greyscale tomographic slices are included for each sample as a visual representation of the change in the microstructure during the respective dynamic sequences. Cumulative bubble size distributions (BND vs. bubble volume) during bubble growth in: (b) LIP and (d) MI samples at different temperatures. Both samples display a range of BNDs and bubble volumes at each

characteristic timescales for diffusion (τ_d) and viscous deformation/relaxation (τ_v) are:

$$\tau_d = \frac{r^2}{D_{\rm H_2O}} \tag{1}$$

$$\tau_{\nu} = \frac{\eta_{\text{melt}}}{\Delta P_g} \tag{2}$$

where $D_{\text{H}_2\text{O}}$ is the H₂O diffusion coefficient or diffusivity (Zhang et al. 2000). η_{melt} is the melt viscosity, and ΔP_g is the gas overpressure. Here, we refer to the closed-system end-member case and calculate ΔP_g using the ideal gas law and the equation of state for H₂O reported in Pitzer and Sterner (1994) (Table 1; see also Pistone 2012). H₂O diffusion in highly viscous rhyolitic melts at low H₂O contents (<<1 wt.%), such as those explored in our study, is extremely

temperature. In the BND analyses, all bubbles more than 0.9 mm from the centre of the sample cylinder are excluded because of boundary effects in the subsequent analysis (Mader et al. 2012). Likewise, bubble diameters smaller than 80 μ m were excluded from the analysis because their behaviour is more erratic and not indicative of the general trends of BNDs; in total 2 % of the data volume was excluded from the analyses

slow ($D_{\rm H_2O} = 8.0 \cdot 10^{-13}$ to $1.4 \cdot 10^{-11}$ m²/s, in the temperature range 883–1253 K; Jambon et al. 1992; below 883 K, any determination of $D_{\rm H_2O}$ is impossible due to the increase of the glass transition temperature of the experimental charges with H₂O removal from the silicic melt during experiments).

In order to determine whether gas exsolution is dominantly controlled by H_2O diffusion *or* gas expansion, the nondimensional Péclet number (Pe), which is the ratio between the characteristic timescales for diffusion (Eq. 1) and viscous deformation/relaxation (Eq. 2), must be determined (Navon et al. 1998):

$$Pe = \frac{\tau_d}{\tau_v} = \frac{\Delta P_g r^2}{\eta_{\text{melt}} D_{\text{H}_2\text{O}}}$$
(3)

In our experiments gas exsolution occurs under conditions of Pe>>1, at temperatures higher than 967 K (Table 1), and in a

Fig. 8 The evolution of bubble size distributions with temperature in the MI sample based on five different size classes: 70, 90, 110, 130, and 150 μ m. Each class has a 20 μ m range, where, for example, the 70 μ m class represents bubbles that have a radius between 50 and 70 μ m. Bubbles larger than the 150 μ m class are not found in the MI sample; bubbles smaller than a 40 μ m radius are excluded from the present analysis as outlined in the caption of Fig. 7



short time interval (<15 s), and, therefore, diffusive mass transfer can be considered unimportant relative to the rate of expansion.

To further examine H₂O diffusion, laboratory time-dependent experiments from previous studies were performed with silicic melts at a specific temperature for different durations of time, ranging from hours to days. The bubble nucleation rate decayed with time because the volume available for progressive nucleation and the degree of H₂O supersaturation at the specified temperature decreased with time (Bagdassarov et al. 1996). In the experiments of Bagdassarov et al. (1996). the time delay for bubble nucleation (also known as induction time or lag time) characterises the capacity of the system to reorganise itself until a steady-state flux of nuclei is generated (Toschev 1973). Conversely, in short duration (<15 s) experiments like those we conducted in this study, with temperatures increasing at a constant rate (15 to 30 K/s) and Pe>>1, H₂O diffusion does not keep up with the temperature increase (i.e. H₂O diffusion is very slow at low H₂O contents in silicic melts; Zhang et al. 1991). and thus, the degree of H₂O supersaturation is expected to increase with time. This may explain the bubble growth "delay" observed in our experiments conducted with bubble-bearing systems (Fig. 6b). Such a bubble growth "delay" should favour H₂O supersaturation of silicate melt, and the resulting η_{melt} should be lower than that computed here (Fig. 4c), due to the presence of supersaturated H₂O. This implies that the degree of H₂O supersaturation may control the kinetics of degassing and the rate of volume expansion of the gas-melt suspension (i.e. the rate of β increase; Mangan and Sisson 2000).

Degassing modalities in bubble-free and bubble-bearing systems

During bubble growth, the β -temperature diagrams (Fig. 6) show different modalities of degassing between samples initially

containing bubbles (MI) and initially bubble-free glasses (LIP). The LIP sample shows two principal segments: (a) initial rapid increase of bubble volume, and (b) gas exsolution at constant β (Fig. 6a). The MI sample displays three main segments: (i) time delay for bubble nucleation accompanied by H₂O flux into the pre-existing gas bubbles; (ii) a vesiculation or β -increase regime; and (iii) a "quasi-steady-state" characterised by constant β (Fig. 6b) due to H₂O exhaustion in the melt (≤ 0.1 wt.%; Fig. 4). In the MI sample, β follows a sigmoidal trend, as predicted by the Avrami equation (Avrami 1939; 1940). but the final true steady-state regime is never achieved (Fig. 6b). Conversely, the LIP sample is characterised by a large release of gas induced by bubble coalescence after the initial rapid increase of β (Fig. 4a). The subsequent "quasi-steady-state" regime, accompanied by only a slight increase of β ($\Delta\beta < 0.2$; Fig. 6a), together with a strong increase of bubble anisotropy at the temperature where the bubble volume increases suddenly (1088 K), confirms the release of gas through gas channels (Fig. 6a). The LGM sample does not display significant vesiculation ($\beta < 0.04$; Fig. 6a); this might suggest that the combination of short experimental duration (<14 seconds), low-H₂O content in the initial glass (≤ 0.1 wt.%), and initial high glass transition temperature (975 K, which then increases during gas exsolution) hampered any considerable vesiculation (Fig. 4a), even in presence of oxides that could have acted as preferential nucleation sites (e.g. Hurwitz and Navon 1994). The CAN sample shows hybrid behaviour between the LIP and MI samples. Indeed, the CAN sample displays an initial sharp increase in β up to 0.6 (Fig. 6b), followed by a slow increase up to 0.74 (= β_{max}) in a "quasi-steady-state" manner, with no evident bubble coalescence, which is also confirmed by the lack of H₂O released during KFT analyses (Fig. 4b). Overall, the behaviour of the CAN sample is similar to that of the MI sample, except for the initial onset of vesiculation, which is similar to the LIP sample.

Lii sai	nple										
$T(\mathbf{K})$	β	Apparent H ₂ O (wt.%)	$\text{Log } \eta_{\text{melt}} (\text{Pa} \cdot \text{s})$								
1073	0.00	0.00	8.45								
1088	0.35	0.35	9.18								
1103	0.34	0.35	8.94								
1118	0.33	0.36	8.74								
1133	0.34	0.36	8.52								
1148	0.37	0.37	8.33								
1163	0.41	0.38	8.15								
1178	0.41	0.39	7.98								
1193	0.40	0.40	7.81								
1208	0.41	0.41	7.64								
1223	0.43	0.42	7.49								
1238	0.45	0.43	7.33								
1253	0.48	0.44	7.18								
1268	0.48	0.45	7.04								
MI san	nple										
$T(\mathbf{K})$	β	Apparent H ₂ O (wt.%)	$\text{Log } \eta_{\text{melt}} (\text{Pa} \cdot \text{s})$	$r(\mu m)$	<i>r</i> ′ (µm/s)	ΔP_{g} (MPa)	$D (H_2O) (\mu m^2/s)$	$l_{c}\left(\mu m\right)$	$\tau_{d}\left(s\right)$	$\tau_{v}\left(s\right)$	Pe
											0
907	0.02	0.10	11.49	93	2	1.11	0.11	0.33	8E+04	3E+05	0
907 937	0.02 0.02	0.10 0.10	11.49 10.80	93 95	2 4	1.11 1.24	0.11 0.16	0.33 0.40	8E+04 6E+04	3E+05 5E+04	0 1
907 937 967	0.02 0.02 0.02	0.10 0.10 0.11	11.49 10.80 10.22	93 95 99	2 4 3	1.11 1.24 0.83	0.11 0.16 0.24	0.33 0.40 0.49	8E+04 6E+04 4E+04	3E+05 5E+04 2E+04	0 1 2
907 937 967 997	0.02 0.02 0.02 0.05	0.10 0.10 0.11 0.12	11.49 10.80 10.22 9.68	93 95 99 102	2 4 3 1	1.11 1.24 0.83 0.67	0.11 0.16 0.24 0.35	0.33 0.40 0.49 0.59	8E+04 6E+04 4E+04 3E+04	3E+05 5E+04 2E+04 7E+03	0 1 2 4
907 937 967 997 1027	0.02 0.02 0.02 0.05 0.10	0.10 0.10 0.11 0.12 0.12	11.49 10.80 10.22 9.68 9.14	93 95 99 102 103	2 4 3 1 2	1.11 1.24 0.83 0.67 0.69	0.11 0.16 0.24 0.35 0.51	0.33 0.40 0.49 0.59 0.71	8E+04 6E+04 4E+04 3E+04 2E+04	3E+05 5E+04 2E+04 7E+03 2E+03	0 1 2 4 10
907 937 967 997 1027 1057	0.02 0.02 0.02 0.05 0.10 0.20	0.10 0.10 0.11 0.12 0.12 0.14	11.49 10.80 10.22 9.68 9.14 8.72	93 95 99 102 103 105	2 4 3 1 2 2	1.11 1.24 0.83 0.67 0.69 0.91	0.11 0.16 0.24 0.35 0.51 0.73	0.33 0.40 0.49 0.59 0.71 0.86	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02	0 1 2 4 10 26
907 937 967 997 1027 1057 1087	0.02 0.02 0.02 0.05 0.10 0.20 0.33	0.10 0.10 0.11 0.12 0.12 0.14 0.14	11.49 10.80 10.22 9.68 9.14 8.72 8.25	93 95 99 102 103 105 107	2 4 3 1 2 2 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04	0.11 0.16 0.24 0.35 0.51 0.73 0.99	0.33 0.40 0.49 0.59 0.71 0.86 1.00	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02	0 1 2 4 10 26 68
907 937 967 997 1027 1057 1087 1117	0.02 0.02 0.02 0.05 0.10 0.20 0.33 0.48	0.10 0.10 0.11 0.12 0.12 0.14 0.14 0.15	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84	93 95 99 102 103 105 107 108	2 4 3 1 2 2 1 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01	0 1 2 4 10 26 68 125
907 937 967 997 1027 1057 1087 1117 1147	0.02 0.02 0.02 0.05 0.10 0.20 0.33 0.48 0.62	0.10 0.10 0.11 0.12 0.12 0.14 0.14 0.15 0.15	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84 7.43	93 95 99 102 103 105 107 108 109	2 4 3 1 2 2 1 1 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04 1.10	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38 1.79	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17 1.34	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03 7E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01 2E+01	0 1 2 4 10 26 68 125 271
907 937 967 997 1027 1057 1087 1117 1147 1177	0.02 0.02 0.05 0.10 0.20 0.33 0.48 0.62 0.67	0.10 0.10 0.11 0.12 0.12 0.14 0.14 0.15 0.15 0.16	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84 7.43 7.08	93 95 99 102 103 105 107 108 109 110	2 4 3 1 2 2 1 1 1 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04 1.10 1.04	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38 1.79 2.32	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17 1.34 1.52	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03 7E+03 5E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01 2E+01 1E+01	0 1 2 4 10 26 68 125 271 453
907 937 967 997 1027 1057 1087 1117 1147 1177 1207	0.02 0.02 0.05 0.10 0.20 0.33 0.48 0.62 0.67 0.77	0.10 0.10 0.11 0.12 0.12 0.14 0.14 0.15 0.15 0.16 0.16	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84 7.43 7.08 6.71	93 95 99 102 103 105 107 108 109 110 111	2 4 3 1 2 2 1 1 1 1 0	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04 1.10 1.04 1.04	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38 1.79 2.32 2.95	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17 1.34 1.52 1.72	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03 7E+03 5E+03 4E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01 2E+01 1E+01 5E+00	0 1 2 4 10 26 68 125 271 453 841
907 937 967 997 1027 1057 1087 1117 1147 1147 1207 1237	0.02 0.02 0.05 0.10 0.20 0.33 0.48 0.62 0.67 0.77 0.84	0.10 0.10 0.11 0.12 0.12 0.14 0.14 0.15 0.15 0.16 0.16 0.17	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84 7.43 7.08 6.71 6.40	93 95 99 102 103 105 107 108 109 110 111 111	2 4 3 1 2 2 1 1 1 1 0 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04 1.10 1.04 1.04 1.04 1.13	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38 1.79 2.32 2.95 3.72	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17 1.34 1.52 1.72 1.93	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03 7E+03 5E+03 4E+03 3E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01 2E+01 1E+01 5E+00 2E+00	0 1 2 4 10 26 68 125 271 453 841 1494
907 937 967 997 1027 1057 1087 1117 1147 1147 1207 1237 1267	0.02 0.02 0.05 0.10 0.20 0.33 0.48 0.62 0.67 0.77 0.84 0.85	0.10 0.11 0.12 0.12 0.14 0.14 0.15 0.15 0.16 0.16 0.17 0.17	11.49 10.80 10.22 9.68 9.14 8.72 8.25 7.84 7.43 7.08 6.71 6.40 6.08	93 95 99 102 103 105 107 108 109 110 111 111 111	2 4 3 1 2 2 1 1 1 1 0 1 1	1.11 1.24 0.83 0.67 0.69 0.91 1.04 1.04 1.04 1.04 1.04 1.04 1.13 1.13	0.11 0.16 0.24 0.35 0.51 0.73 0.99 1.38 1.79 2.32 2.95 3.72 4.72	0.33 0.40 0.49 0.59 0.71 0.86 1.00 1.17 1.34 1.52 1.72 1.93 2.17	8E+04 6E+04 4E+04 3E+04 2E+04 2E+04 1E+04 8E+03 7E+03 5E+03 4E+03 3E+03 3E+03	3E+05 5E+04 2E+04 7E+03 2E+03 6E+02 2E+02 7E+01 2E+01 1E+01 5E+00 2E+00 1E+00	0 1 2 4 10 26 68 125 271 453 841 1494 2526

Table 1Summary of the textural and physical parameters of the MI and LIP samples (see experiments "mi3_Dynamic" and "lip4_Dynamic",respectively; Table 1B in Appendix), selected as a representation for bubble growth in highly viscous bubble-bearing magmas in this contribution

Parameters ΔP_g , D, l_c , τ_d , and τ_v are calculated only in the MI sample where gas permeability is absent

T temperature, β bubble volume fraction, V_{β} total bubble volume, *Apparent H*₂O cumulative extracted H₂O from the cylindrical LIP and MI samples, measured by KFT technique, $Log \eta_{melt}$ logarithm of melt viscosity calculated with the model of Giordano et al. (2008). *r* weighted average bubble radius; *r'* bubble radius growth rate, ΔP_g gas overpressure, D_{H_2O} diffusion coefficient or diffusivity of H₂O (Zhang et al. 2000). l_c diffusion characteristic length, τ_d diffusion timescale, τ_v viscous timescale, *Pe* Péclet number.

(*) = no available data for H_2O from the work of Pitzer and Sterner (1994).

The initial bubble bursting could be related to an initial lower η_{melt} of the phonolitic CAN sample than those of the other rhyolitic samples investigated here (Figs. 1 and 4c; Table 1A in the Appendix).

Gas connectivity in bubble-free and bubble-bearing systems: the importance of the initial presence of gas bubbles in magmas

It is known that gas connectivity occurs when a critical β is achieved (Sahimi 1994). According to the standard

percolation theory, bubbles form an interconnected network when a threshold value of β_c is reached and, beyond that, gas permeability (k) increases with increasing β , following a power-law relationship (Rust and Cashman 2011):

$$\mathbf{k} \propto \left(\beta - \beta_c\right)^b \tag{4}$$

where *b* depends on pore geometry (b=2 as derived from Poiseuille flow and Darcy's law equations; Wright et al. 2009, and references therein). In the standard percolation theory, if uniform spheres are placed randomly in a much larger sample volume and the spheres are allowed to overlap/

connect, a cluster of touching and overlapping spheres will span the sample volume until the critical $\beta_c = 0.29$ is obtained (Sahimi 1994). Following this theory, some studies (e.g. Polacci et al. 2008) assumed that magma becomes permeable when $\beta_c = 0.30$. However, in numerical simulations (e.g. Garboczi et al. 1995) as well as in experimental studies where shear deformation induced bubble coalescence (Okumura et al. 2006, 2008, 2009, 2013). the percolation threshold was reduced by bubble deformation, where oblate objects increased the likelihood of bubble connectivity and outgassing from the magmatic system (Caricchi et al. 2011; Pistone et al. 2012; Shields et al. 2014). Gas exsolution in the LIP sample is consistent with the standard percolation theory, since bubble connectivity is initiated at $\beta = 0.35$ (> $\beta_c = 0.30$) after the initial vesiculation burst at 1088 K (Fig. 6a). In contrast, the percolation threshold is never achieved in systems initially containing bubbles (MI and CAN), where the final bubble content reaches values close to or above the value of maximum packing fraction ($\beta_{\text{max}}=0.74$; Fig. 6b). There are numerous studies testifying that bubble-bearing suspensions can reach $\beta >>$ 0.30 without becoming permeable (e.g. Blower 2001). this suggests that parameters other than the percolation threshold might be important in determining permeability in bubble-rich systems (Okumura et al. 2009).

The striking difference in vesiculation dynamics between the MI (gas expansion) and LIP (gas connectivity) samples demonstrates that Eq. 4 suffers from the limitations of the percolation theory, which does not take into account either the bulk volume increase during vesiculation or the time required to thin the films that separate individual bubbles (Rust and Cashman 2011, and references therein). Therefore, the value of $\beta_{c} = 0.30$ obtained from standard percolation theory provides only the minimum porosity at which connected bubbles may form a permeable network during vesiculation. In contrast to the case of the LIP sample, the MI sample does not achieve gas permeability and outgassing because of the initial presence of gas bubbles prior to heating. In our experiments, the influence of the heating rate is probably not a significant factor determining the conditions of gas permeability versus gas expansion. In fact, MI and CAN samples were heated at different rates (30 K/s in MI and 15 K/s in CAN), but both systems did not experience gas permeability and outgassing (Fig. 6b). The results of this study indicate that the presence or absence of initial gas bubbles in the system is an important factor in determining the occurrence of gas connectivity in magmas. In the absence of gas bubbles and other initial heterogeneities (e.g. crystals and/or large chemical heterogeneities in the melt), nucleation of bubbles can theoretically occur everywhere in the melt domain. This would increase the probability of connectivity between neighbour bubbles nucleating and growing over a short distance ($<3 \mu m$). Conversely, the initial presence of gas bubbles, combined with the initial spatial distribution of bubbles (i.e. distance between bubbles is >10 μ m in MI and CAN samples), drives gas exsolution to pre-existing sites that will unlikely connect. Therefore, we can say that: (i) in bubble-free magmas, bubble connectivity may follow the general principles of the percolation theory; and (ii) conversely, in bubble-bearing systems, bubble connectivity could be hampered and magmas can expand well beyond the percolation threshold without becoming permeable.

It is also known that bubble connectivity is a function of the surface tension between gas and surrounding melt, which, in turn, depends on temperature, pressure, H₂O content of the melt phase, and η_{melt} (Bagdassarov et al. 2000; Mangan and Sisson 2000; Gardner and Ketcham 2011). However, the data acquired in this study do not allow for estimations of surface tension nor its potential correlation with the vesiculation process observed in H₂O-poor (<<1 wt.%) silicic melts during the X-ray tomographic microscopy experiments.

Conclusions

Our results highlight how pre-existing gas bubbles may strongly affect the dynamics of vesiculation (bubble nucleation, growth, coalescence and outgassing) in a silicic magmatic system. Crystal-free, volatile-undersaturated magmas (i.e. no initial gas bubbles) show localised nucleation and growth of bubbles (heterogeneous vesiculation driven by the chemical heterogeneities in the initial glass? homogeneous bubble nucleation, growth, and coalescence occurring almost simultaneously?), which tend to coalesce and generate permeable pathways for gas escape at >30 vol.% gas content, following the predictions of the standard percolation theory. Conversely, when a crystal-free magma is volatile-saturated (i.e. presence of initial gas bubbles), gas exsolution is controlled by the existence of bubbles in the magmatic system prior to heating, and magmas can extensively expand without the development of bubble connectivity and outgassing. It is important to bear in mind that samples used in this study are initially H₂O-poor (<<1 wt.%) due to the imposed experimental conditions (high-temperature experiments conducted at room pressure). Moreover, our experiments were conducted with heating, thereby melt viscosity decreases with time.

In a natural scenario, magma residing in a shallow reservoir (≤ 6 km) is expected to be richer in H₂O dissolved in the melt (≤ 4 wt.%), and, during its ascent, that magma should experience decompression and relative cooling. The vesicularities obtained in our experiments match those found in natural samples. However, the bubble number densities presented are much lower than those observed in natural volcanic vesicular samples. Therefore, at the present stage, our experimental results provide qualitative insights into the processes of bubble nucleation and growth occurring in resident and ascending magmas. But our results also underline the importance of the initial presence *or* absence of gas bubbles, which appears to

have a significant impact on the modality of degassing in a magma stored in a reservoir or ascending in a volcanic conduit. The principal difference in degassing behaviour observed in this study could imply that eruptions fed by magmas that are volatile-saturated already in the magma chamber have a higher probability of being explosive than eruptions associated with resident volatile-undersaturated magmas.

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